Heat Consumption Assessment of the Domestic Hot Water Systems in the Apartment Buildings

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Abstract – This study presents the analysis of energy consumption for domestic hot water in apartment buildings in Riga, Latvia. The aggregate data contains information about 39 apartment buildings, including heat energy consumption and domestic hot water (DHW) consumption. The analysis is focused on the heat energy consumption and seasonal characteristics in the DHW system.

The analysis characterizes the DHW consumption, energy consumption for DHW and energy losses in the DHW systems in apartment buildings.

Keywords – Apartment buildings, domestic hot water (DHW), heat consumption, heat gains and heat losses.

I. INTRODUCTION

The energy consumption of DHW needs of households and some other building sectors constitutes a significant part of the building's energy balance.

The building energy efficiency improvement measures reduce the heating energy required proportion and logically increase the share of energy consumption for DHW needs. It is likely that the production and distribution of DHW in buildings will constitute a dominant share of both the present, and in particular, the future energy design requirements of buildings. [1]

Previously studies carried out in various European countries [2], [3], [4], China [5], [6], Japan [7], [8], [9], USA [10], [11], Canada [12] points the many differences in DHW consumption as well as the tendency to change over time due to a global increase of energy prices, changes in technologies, introducing of individual metering, as well as wide variety of other factors that may appear on local or regional level.

Measurements in Denmark documented not only a relatively high energy consumption for DHW in apartment buildings, but also recorded surprisingly large heat losses from the DHW circulation lines [13], [14]. Recent investigation of 24 buildings in Danmark shows that most of the energy demand for DHW is lost in the circulation system. The efficiency was 0.30–0.77 (heat loss 23–70%) in apartment buildings and efficiency 0.11– 0.46 (heat loss 54–89%) in office buildings. [1]

The Energy Performance of Buildings Directive (EPBD) [15] in the version of 2010, the so-called recast EPBD, demands in annex I 'Common general framework for the calculation of energy performance of buildings (referred to in Article 3)' that '(1) the energy performance of a building shall be determined on the basis of the calculated or actual annual energy that is consumed in order to meet the different needs associated with its typical use and shall reflect the heating energy needs and cooling energy needs (energy needed to avoid overheating) to

maintain the envisaged temperature conditions of the building, and domestic hot water needs'. This is one of essential requirements already established by the EPBD in the version of 2002 [16].

In Latvia, EPBD requirements have been transposed by the Law on the Energy Performance of Buildings (13th March 2008, recast 6th December 2012). The calculation procedures are prescribed by the Cabinet Regulation on the Calculation of Energy Performance of Buildings (No. 348 as of 25th June 2013 replace previous No. 39 as of 13th January 2009).

The structure that should be used for the calculation of energy use in space heating systems and domestic hot water systems in buildings is specified in standard EN 15316-1 [17].

The objective of the calculation is to contribute to the evaluation of the annual energy use of the space heating and domestic hot water systems. If there is seasonal heating in the building, the year should at least be divided into two calculation periods, i.e., the heating season and the rest of the year. Different levels of detail may be used for the different subsystems of the heating system. However, it is essential that the results correspond to the defined output values of the subsystem: – energy input; – energy output; – system thermal losses; – recoverable system thermal losses; – auxiliary energy; in order to ensure proper links to calculations for the following sub-systems and development of a common structure. [18]

According to the CEN standards, the energy consumption for domestic hot water (DHW) production is calculated using a three-step approach: 1) building DHW needs, 2) distribution and 3) generation. The correct estimation of the domestic hot water needs is essential. This results in volume and time of hot water needs throughout the year (the gross hot water demand) and tapping patterns. Tapping patterns are important for the calculation of distribution and generation losses. Also the estimation of the contribution of each heat generator (e.g., thermal solar) depends on the tapping patterns. The second step comprises the calculation of the distribution systems. This part of a domestic hot water system is all between the generation system and the point of tapping. Important aspects to be considered in this respect are heat losses and pump energy. The distribution losses can be higher than the domestic hot water needs. The gross hot water needs are delivered by heat generators. There are several types of generators available, and many of them are also used to provide space heating. Space heating and domestic hot water have some distinctively different properties, so there are separate standards on DHW and space heat generation. DHW is different from space heating in that the heat demand has an interval character and a different temperature level [19].

The correct characterization of hot water needs is important because the losses of boilers and the distribution system are very sensitive to the couple of frequency and energy content of heat up and cool down at any tapping. Therefore, the needs are defined by the energy amount and also by the tapping patterns. The energy amount of hot water needs could represent about 25% of the final heating needs (or 20 to 25 kWh/m² per year) in existing residential buildings. The percentage of hot water needs increases in well-insulated houses [20].

The standard EN 15316-3-1 [21] gives four methods for calculation of the energy needs of the delivered domestic hot water:

-energy need related to tapping programs,

-energy need related to volume needs,

-energy need linear with floor area,

-energy need from tabulated values for different building types or functions.

For all methods a national annex is required. The annexes to the standard provide default values. Countries need to decide which method they prefer and which specific energy need, depending on a building type, is suitable.

The EN 15316-3-2 [22] gives methods for calculation of heat losses, the recoverable heat losses and the auxiliary energy of the domestic hot water distribution system.

Domestic hot water distribution systems may consist of a circulation system and/or distribution pipes. Distribution pipe losses are dominated by the heating up and cooling down of the pipes at any tapping, so these losses are sensitive to the tapping pattern [23].

The standard gives five calculation methods for distribution pipe losses:

- heat losses related to floor area,
- heat losses related to pipe lengths simple method,
- heat losses related to pipe lengths tabulated data method,
- heat losses related to tapping pattern,

- heat losses based on detailed calculation method.

Circulation systems are in general operated at constant temperature. Therefore circulation system losses do not depend on tapping patterns. Loss reduction may be achieved by applying pipe insulation and night set-back.

The standard gives the following methods to calculate circulation system losses:

- heat losses related to circulation pipe length,
- heat losses based on detailed calculation method,
- heat losses while circulation is off.

The total heat losses are the sum of distribution pipe losses (no circulation loop) and circulation system losses (collective part with circulation loop). Also methods are given to determine auxiliary energy consumption for:

- pumps for circulation systems,
- ribbon or trace heating.

For all methods a national annex is required. The annexes to the standard provide default values.

Dwelling houses are one of the largest district heat users in Latvia. In 2010, Latvian households consumed 70% of all district heat energy produced [24].

Estimates based on the data aggregated by district heating supplier JSC "Rīgas Siltums" on heat consumption of more than 5,000 residential buildings in Riga city shows that the amount of energy consumed in hot water systems represents an average of 50.9 kWh per square meter of heated apartments annually (fig. 1) or 27% of the total heat energy consumption in those buildings.



Fig. 1. Yearly consumption of heat energy for heating and DHW needs in apartment buildings connected to district heating in Riga.

Usually apartment buildings have a single heat meter for both heating and DHW in Latvia. Therefore, if the calculation of energy performance of buildings is carried out, the energy use for heating, DHW consumption, circulation loop and others should be assessed separately.

Analysis of the data gives the base to develop methodology for assessment of energy performance of DHW systems adapted for national (Latvia) level.

II. METHODS

The authors have analysed the heat energy consumption and water consumption in apartment buildings in Plavnieki and Purvciems area in Riga in the year 2011.

The aggregate data contained information on 39 buildings with 3167 households and total heated area of 158189 m² in Riga. The total population in these buildings is 7139 inhabitants. The Buildings were constructed by standardized design types from 1966 to 1988; the average heated area of buildings is 3164 m². Average area per person is 22.3 m². Buildings have 5 to 12 floors and 1 to 6 sections. Usually each section of the building has separate entrance and similar design with other sections. The characteristics of buildings are given in table 1.

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Type of standar d design	Number of building s	Year of constructio n	Numbe r of floors	Averag e number of flats	Average area of building s m ²	Averag e area of flats, m ²	Average number of inhabitant s	Average area per inhabitant , m ²	Numbe r of section s	Length of section , m	Width of section , m	Number of circulatio n loops in section
316	2	1966	5	70	2764	39.5	138	20.5	4	15.7	11.0	3
464A	7	1969-1977	5	54	2535	47.8	127	20.0	3 or 4	13.5	11.5	3
104/m	2	1987	5	74	2655	35.5	130	20.6	4	13	15	4
602	15	1971-1988	9	113	3363	53.2	267	22.0	1 to 6	25.6	11.2	6
467A	7	1977-1987	9	54	2838	52.3	124	22.7	1 to 3	25.6	11.1	6
104	5	1979-1981	12	71	3910	54.8	141	27.8	1	32	15	6

TABLE 1 THE CHARACTERISTICS OF THE TYPES OF APARTMENT BUILDINGS

Investigated buildings are connected to the district heating network of JSC "Rīgas Siltums". All buildings have the automatic heating `unit equipped with the heat counters, as well as hot and cold water meters. The measuring equipment belongs to "B" class meter with error limit ± 3 percent. There is no separate heat metering for heating and DHW. The draw of DHW system is shown on figure 2.



Fig. 2. The DHW circulation system for apartment buildings. (HE - heat exchanger)

III. RESULTS

General water consumption characteristics

For part of buildings have both data for DHW and DCW. The average total water consumption in the 22 investigated buildings in Riga is 3.64 litres per m² per day annually, of which 1.52 DHW and 2.12 cold water. The consumption of domestic cold water and domestic hot water per m² per day is shown in Fig. 3.



Fig. 3. Daily consumption of domestic cold water (DCW) and domestic hot water (DHW) in apartment buildings (litres per m² per day).

To achieve the objective of the study, the authors have analysed data on DHW consumption and heat consumption in the DHW system.

Average annual DHW consumption ratio is 42% of total consumption. Fig. 4 shows DHW consumption ratios and variations per month.



Fig. 4. The ratio (%) of consumption of domestic hot water to the total consumption in apartment buildings per month

Figure 5 shows the variations ratio of DHW, DCW and total water consumption against the relevant annual average.



Fig. 5. The variations ratio of DHW, DCW and total water consumption against the relevant annual average.

DHW consumption characteristics

The study shows specific DHW indicators on the heated area per household and per person (Table 2) and correlation of DHW consumption of these indicators (Figures 6–8). The most accurate data on DHW consumption is per person (Fig. 8).

TABLE 2

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	Minimum	Maximum	Average	R- squared value			
DHW daily consumption, litres per day							
- per m ²							
Riga	1.10	2.73	1.86	0.880			
Reference values* (Riga)	1.13	1.48	1.32	-			
- per household							
Riga	55.7	142.6	92.8	0.866			
Reference values**	Reference100.2 (tapping program No 2)values**199.8 (tapping program No 3)						
- per person							
Riga	24.2	60.2	41.0	0.946			
Reference 36.0 (tapping program No 1) value***							
* calculated accordin ** A.2 and A.3 of an *** A.1 annex A of s	ng B.2 of annex nex A of stand standard EN 15	B of standard ard EN 15316- 316-3-1	EN 15316-3- 3-1	1			

By comparing DHW daily consumption indicators to default values set out in Annex A "Tapping Program for Single Family Dwellings" of standard EN 15316-3-1, the authors have found out that average DHW daily consumption of 41.0 litres per person per day is close to the default value of 36 litres per person per day, determined in Table A.1 'Tapping program No. 1'. Taking into account that the standard default value is set for equivalent hot water litres at 60°C, average DHW daily consumption in the investigated buildings with the temperature correction from 50°C to 60°C would be closer to the standard value.

DHW daily consumption maximum value of 76.2 litres per household is less than default values of 100.2 litres per dwelling, determined in Table A.2 ('Tapping program No. 2.') and is very different from the default value of 199.8 litres per dwelling, determined in Table A.3 ('Tapping program No. 3.').



Fig. 6. Correlation of DHW consumption (m³) to heated area (m²) (39 buildings in Riga)



Fig. 7. Correlation of DHW consumption (m^3) to the number of households (39 buildings in Riga)



Fig. 8. Correlation of DHW consumption (m³) to the number of inhabitants (39 buildings in Riga)

In addition, the study shows that DHW consumption differs by season:

- 94% of yearly average consumption in the non-heating period (May-September),

- 106% of yearly average consumption in the heating period (November–March).

Data on October and April are not taken into account because heating is started or stopped in these months.

Seasonal DHW consumption variations are identified in other researches [12], [25], [26]. Significant factor which affects the consumption of DHW is variation of supplied cold water temperature during the year.

Total heat consumption in the investigated buildings is from 164 to 225 (average 189) kWh per m^2 per annum.

To determine the energy consumption for DHW consumption and DHW circulation loop, the authors used data on energy consumption and DHW consumption in the non-heating period (May–September).

The energy consumption Q_w for DHW heating for a period is calculated as follows (1):

$$Q_{w} = V \frac{\rho_{w} C_{w}}{3600} \cdot \left(\theta_{w,del} - \theta_{w,o}\right) \qquad (1)$$

where Q_w – the energy consumption for DHW heating, kWh; V – the DHW consumption per period, m³; ρ_w – the water density at temperature $\theta_{w,o}$, kg/m³; C_w – the water specific heat capacity, J/kg K; $\theta_{w,del}$ – the temperature of cold water (°C); $\theta_{w,o}$ – the temperature of DHW (°C); 3600 – number to take into account for conversion from mega joules to kilowatt hours.

In the investigated buildings, the delivered temperature of cold water ranges from 5 to 15 °C during the year; temperature of heated water from heat exchanger ranges from 50 to 55 °C (the temperature drops on circulation loop about five to ten degrees, in the calculation used temperature difference is 40

degrees). Energy consumption necessary to heat 1 m^3 of cold water depending on the temperatures difference are shown on table 3. The variations of energy consumption depending the deviation of average temperature shown the error margin of energy needs for DHW consumption.

The energy consumption for DHW needs varies from 18.8 to 46.3 and average is 33.0 kWh per m^2 annually in investigated apartment buildings.

TABLE 3
HEAT CONSUMPTION DEPENDING ON DIFFERENCE OF INLET AND HEATED
WATER TEMPERATURE

Temperatu re of the inlet cold water.	Temperatures difference if average temperature of DHW	The energy content for heating of 1m ³ of cold	The variations of energy consumption depending deviation from average temperature (40 degrees)		
°C	circulation loop is +50 °C, degrees	water, kWh per 1m ³	kWh per 1m ³	percentage	
+6	44	50,4	+4.6	+10%	
+8	42	48,1	+2.3	+5%	
+10	40	45,8	0	-	
+12	38	43,6	-2.2	-5%	
+14	36	41,3	-4.5	-10%	



Calculation results of heat energy average values per m^2 of heated area per month are shown in Fig. 9.

Fig. 9. Heat energy average values per m² of heated dwelling area per month

During the heating season DHW circulation loop losses is recoverable for heating needs. Thus the losses from DHW system is heat gains for whole building during heating season.

During the non-heated season, the ratio of DHW circulation loop losses in the investigated buildings ranges from 35 to 79% from total heat consumption, and the average loss ratio is 56%.

The DHW circulation losses in most cases range from 12.9 to 23.0 kWh per m² in the investigated buildings during the non-heating season. There are two extremely different results (5.3 and 32.1 kWh per m²), which are outside normal values. Average DHW circulation losses are 18.0 kWh per m², 0.97 MWh per households during the non-heating season (Table 4).

 TABLE 4

 HEAT LOSSES FROM DHW CIRCULATION LOOP INDICATORS

	Heat losses from DHW circulation loop during the non-heating season			
	Minimum	Maximum	Average	
kWh per m ²	12.9	23.0	18.0	
MWh per household	0.53	1.42	0.94	

The evaluation of DHW circulation losses correlation to the heated area and to the number of households showed that more

accurate data can be obtained from the heated area (Figures 10–11).

In addition, the authors have compared DHW circulation losses by different building characteristics. The study shows that DHW circulation losses does not markedly depend on heat consumption for DHW needs (Figure 12), number of apartments, inhabitants, storeys in building.





Fig. 11. Correlation of DHW circulation losses to the number of households

Fig. 10. Correlation of DHW circulation losses to the heated area (m²)



Fig. 12. Heat consumption for DHW needs and DHW circulation losses arranged by the space area of households

Assessment of DHW cirulation losses

The authors carried out a comparison of different calculation models for assessment of thermal losses of DHW circulation loop:

- estimation based on metered heat and DHW consumption data on non-heating season (the method and results described above);
- Calculation of thermal losses from circulation loop based on physical approach according to standard EN 15316-3-2.
- Calculation of thermal losses from circulation loop based on physical approach according to standard EN 15316-3-2 using default values from annex D of the standard.

The general determination of thermal losses of a circulation loop comprising a number of pipe section i is given by:

$$Q_{w,dis,ls,col,on} = \sum_{i} U_{W,i} \cdot L_{W,i} \cdot \left(\theta_{W,dis,avg,i} - \theta_{amb,i}\right) \cdot t_{W}$$
⁽²⁾

 $Q_{w,dis,ls,col,on}$ - the linear transmittance of pipe section *i* during period of circulation, Wh/period, $U_{w,i}$ - the linear thermal transmittance of pipe section *i* (W/mK), $L_{w,i}$ - the length of pipe section *i* (m), $\Theta_{w,dis,avg,i}$ - the average

hot water temperature of pipe section i (°C), $\Theta_{amb,i}$ – the average ambient temperature around pipe section i (°C), t_w – calculation period at the corresponding temperature, $\Theta_{w,dis,avg,i}$ (h/period),

(indices: W – domestic hot water, dis – distribution, ls – losses, col – circulation loop (collective), avg – average, amb – ambient)

The DHW circulation system of investigated buildings has the following features:

- vertical distribution with known number of circulation loops in building section for each building type;
- the circulation loops run continuously all the time;
- each apartment has one towel rail on the circulation loop.

Thus authors have work out unified formulas for calculation of length of circulation loop sections for investigated buildings (Table 5). The domestic hot water distribution system comprises three different pipe sections (figure 13):

- distribution from the heat exchanger to the vertical supply pipes on basement (section L_V),
- main supply pipes on heated area comprise: vertical pipes (section L_{S1}) and individual towel rails (section L_{S2}),

- the individual branching pipes to the user outlets on dwellings. Losses from individual branching pipes are not part of circulation loop and losses are part of DHW consumption.



Fig. 13. Location of pipe sections. (HE - heat exchanger)

To calculate thermal losses from circulation loop based on physical approach authors used values given in table 5.

 TABLE 5

 Actual input values used to calculate DHW circulation losses

Pipe section	V	S1	S2		
Pipe characteristics	insulated, steel	non-insulated, steel, DN20/DN25	non-insulated, steel, DN40/DN50		
Linear thermal transmittance of pipe section (W/m·K)	0.4	1	2		
Length of pipe section (m)	$L_{V} = 2 \times L_{B} + B_{B} \times n_{B,dis,col}$ $L_{S,1} = 2 \times L_{B} \times n_{f} \times h_{f} \times n_{B,dis,col}$ $L_{S,2} = n_{dwelling} \times L_{towel rail}$				
The average hot water temperature of pipe section (°C)	50				
The average ambient temperature around pipe section (°C)20 (during non-heating season)		20			
The calculation period (h/period),	24 x 153 days (May-September)				

 $L_{\rm V}, \, L_{\rm S1}, \, L_{\rm S2}$ – the length of pipe sections $L_{\rm V}, \, L_{\rm S1}, \, L_{\rm S2}$ (m), $L_{\rm B}$ –the largest extended length of the building (m), $B_{\rm B}$ – the largest extended width of the building (m), n_f – the number of heated storeys; $n_{B,dis,col}$ – the number of circulation loops in building; h_f – the height of the heated storeys (m), $n_{dwelling}$ – the number of dwellings in building; $L_{towel\ reil}$ - avarage length of the towel rails in dwellings (m).

Indices: B – building, col – circulation loop (collective), dis – distribution, f – floor, W – domestic hot water

The value used on calculation (table 5) differs from the default values given in standard EN 15316-3-2 (Annex D). Default values for calculation of circulation loses (table 6).

TABLE 6
AULT INPUT VALUES TO CALCULATE DHW CIRCULATION LOSSES
ACCORDING TO ANNEX D OF THE STANDARD EN 15316-3-2

DEFA

Pipe section	V	S
Pipe characteristics	insulated	non-insulated pipes exposed
Linear thermal transmittance of pipe section, W/mK	0.4 (buildings up to 1980)	Depending on building area A: 1.0 (A≤200m ²) 2.0 (200 <a≤500m<sup>2)</a≤500m<sup>

		3.0 (A>500m ²)*				
Length of pipe section, m	$L_V = 2 \times L_B + 0.0125 \times L_B \times B_B$ $L_S = 0.075 \times L_B \times B_B \times n_f \times h_f$					
The average hot water temperature of pipe section (°C)	60					
The average ambient temperature around pipe section (°C)	22 (during non- heating season)	22				
Ly, L_S – the length of pipe sections L_V , L_S (m), L_B – the largest extended length of the building (m), B_B – the largest extended width of the building (m), n_f – the number of heated storeys; h_f – the height of the heated storeys (m); Indices: B – building, f – floor						

As the authors are given actual values for the average hot water temperature of pipe sections, the average ambient temperature around pipe section and the calculation period, as an alternative, the authors carried out a calculation of thermal losses from circulation loop using default values of annex D of standard 15316-3-2 only for calculation of length of pipe sections and values for linear thermal transmittance of pipe sections.

According to the standard the linear thermal transmittance of pipe section depends on building area. The calculations with default values of the linear thermal transmittance (3.0 W/m K) of main supply circulation pipe section on heated area of building give results which significantly several times differ from the result of actual assessment.

Thereby authors used input value 1.0 $(W/m \cdot K)$ for calculation of the linear thermal transmittance of main supply circulation pipe section on heated area of building.

The results of calculation by all three methods are shown in figure 14 and table 7.

The authors have found out that heat losses from DHW circulation loop differ by type of standard design. The authors assume that estimation of heat losses from DHW circulation loop based on metered heat and DHW consumption data is a sufficiently accurate.

The calculation of thermal losses from circulation loop based on physical approach both authors model and standard default model in most cases gives significantly higher values than estimation based on metered heat and DHW consumption data.

The results given by the author's methods give closer result to metered data. By design type of buildings the authors calculation model differ from 5% to 85% (average 36%) comparing to estimation based on metered heat and DHW consumption data, meanwhile calculation based on default standard values with adoption for actual conditions differ from 30% to 142% (average 74%).

The authors assume that the difference of calculation is due to inaccurate assumption of values of linear thermal transmittance of pipe sections. This incorrectness can be due to more or less part of pipes is located in the internal structures of buildings, which reduce the heat transfer from pipes to ambient space of building.

The authors believe that this circumstance could take into account by the correction of linear thermal transmittance of pipes. However research data shows that correction factor could be significantly different for different design types of buildings.



Fig. 14. Calculation results for circulation losses by different assessment methods.

Assessment result Calculation on physical approach Type of for design type Authors model Default standard model standard Number min max average differ from design of differ from kWh kWh kWh kWh kWh average (number of floors assessed per m2 per m per m² per m² per m² assessed buildings) result, % result, % 316 (2) 5 13.3 14.2 13.7 25.4 33.2 +142 +8517.5 32.1 21.0 21.8 464A (7) 5 +926.1 +30104 (2) 17.2 17.4 17.3 30.0 +74 +1015 34.8 602 (15) 9 12.9 22.9 18.0 25.2 +3831.7 +73467A (7) 9 16.0 20.017.8 27.0+5133.3 +8612 23.0 20.0 22.8 +1533.7 104(5)17.3 +7024.7 32 1 Average (38) 133 18.3 +3631.6 +74

TABLE 7

DHW CIRCULATION LOSSES BY VARIOUS TYPES OF APARTMENT BUILDINGS DURING THE NON-HEATING SEASON

In addition the authors assessed circulation heat losses ratio by pipe sections. For this assessment author used calculation model on physical approach with the actual input values (table 8) except the average ambient temperature around pipe section in unheated basement on heating season ($\pm 10^{\circ}$ C).

 TABLE 8

 DHW circulation losses ratio by pipe sections

		Circ	ulation y pipe	losses section	ratio 1s		
	Pipe section	V	S1	S2	V	S1	S2
Type of standard design		Non-heating season		Heating season		g I	
316	5	11	56	33	13	55	32
464A	5	12	57	32	14	55	31
104	5	10	60	31	12	58	30
602	9	12	67	22	14	65	21
467A	9	12	64	24	15	62	23
104	12	10	64	26	12	62	26

The study shows that the rate of circulation heat losses on unheated basement varies 10 to 12 % during non-heating season and 12 to 15 % during heating season.

The rate of circulation heat losses of vertical distribution circulation loop pipes and individual towel rails varies depending on the number of floors in the building. Depending of season the rate of circulation heat losses of vertical distribution circulation loop pipes varies 55 to 60 % for 5 floor buildings and 62 to 67 % for 9 or 12 floor buildings. Whereas the rate of circulation heat losses of individual towel rails varies 30 to 33 % for 5 floor buildings and 21 to 26 % for 9 or 12 floor buildings.

IV. CONCLUSION

The study clearly demonstrates that making assessment of energy performance of collective DHW system of apartment buildings, the energy needs for DHW system should be divided into energy for DHW consumption needs for inhabitants and energy for distribution losses.

the study shows that the energy consumption for the energy for DHW consumption needs depend on the number of inhabitants while energy losses for distribution including collective circulation loop depends on distribution pipes length and pipes thermal characteristics.

The energy consumption for DHW needs varies from 18.8 to 46.3 and average is 33.0 kWh per m² annually in investigated apartment buildings.

The study shows that DHW consumption in the apartment buildings most accurate correlated based on the number of inhabitants and less accurate correlated by the number of flats and by the heated area. The DHW consumption varies by season in apartment buildings. DHW consumption was 94% of yearly average in the non-heating period (May–September) and 106% of yearly average in the heating periods (November–March). In order to obtain more precise results it may be taken into account when evaluating energy consumption of DHW system in residential buildings.

The energy losses for DHW distribution including collective circulation loop ranges from 12.9 to 23.0 and average is 18.0 kWh per m^2 in investigated apartment buildings during nonheating season. These indicators can be applied to full year as the energy losses for circulation loop is recoverable during heating season exclude losses from distribution pipes on unheated basement.

The DHW system circulation losses depend on distribution pipes length and pipes thermal characteristics. In addition, in this study it is shown that heat losses from DHW circulation loop differ by different design types. The study shown that DHW circulation losses does not markedly depend on heat consumption for DHW needs, number of apartments, inhabitants or storeys in apartment building but correlation of DHW circulation losses to heated area is significant.

The study has also detected that some consumption characteristics of DHW for apartment buildings are different from the values given in the standard EN 15316-3-1 (Heating systems in buildings – Method for calculation of system energy requirements and system efficiencies – Part 3-1: Domestic hot water systems, characterisation of needs (tapping requirements)); therefore, the standard should be specified in national annexes. The appropriate national annexes of EPBD standards for DHW systems are not developed in Latvia.

The authors believes that calculation of DHW circulation losses should be based on physical approach according to standard EN 15316-3-2 and with nationally adapted default values. The calculations result based on physical approach should be validated with assessment based on measured data of heat and DHW volume consumption since the linear thermal transmittance of pipe section, the average hot water temperature of pipe section, the average ambient temperature around pipe section have significant impact to the calculation results.

The assessed DHW circulation heat losses ratio by pipe sections has shown the potential to save losses on DHW circulation pipe sections.

The DHW circulation losses from main vertical pipes on heated area rate 55 to 67 % of the total. These sections of pipes are not insulated but it is recommended to do it in future.

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REFERENCES

 B. Bøhm, Production and distribution of domestic hot water in selected Danish apartment buildings and institutions. Analysis of consumption, energy efficiency and the significance for energy design requirements of buildings, Energy Conversion and Management 67 (2013) 152-159. http://dx.doi.org/10.1016/j.enconman.2012.11.002

- [2] K. Yliniemi, J. Delsing, J. van Deventer, Experimental verification of a method for estimating energy for domestic hot water production in a 2stage district heating substation, Energy and Buildings 41 (2009) 169– 174. <u>http://dx.doi.org/10.1016/j.enbuild.2008.08.008</u>
- [3] L. Gullev, M. Poulsen, The Installation of Meters Lead to Permanent Changes in Consumer Behaviour, News from DBDH, No. 3, 2006.
- [4] T.A. Koiv, A. Toode, Trends in domestic hot water consumption in Estonian apartment buildings, in: Proceedings Estonian Acad. Sci. Eng., 2006.
- [5] C. Kan, H. Yoshino, et al., 2007. Field survey on heating/cooling loads and end-use energy consumption in China. Summary of SHASE Annual Meeting, 387–390.
- [6] S. Hokoi, D. Ogura, X. Fu, Y. Rao, Field survey on energy consumption due to hot water supply and cooking in Nanjing and Hefei, China, Frontiers of Architectural Research (2013) 2, 134–146. <u>http://dx.doi.org/10.1016/j.foar.2013.03.001</u>
- [7] T. Inoue, S. Mizutani, T. Tanaka, 2006. Energy consumption in housing on the basis of national scale questionnaire: analysis of influence of various factors on annual energy consumption Part2. Journal of Environmental Engineering, Architectural Institute of Japan 606,75–80 Aug.2006.
- [8] Y. Hasegawa, T. Inoue, 2004. Energy consumption in housing on the basis of national scale questionnaire: study on influence of residential characteristic and dispersion of energy consumption Part 1. Journal of Environmental Engineering, Architectural Institute of Japan 583,23–28 Sep.2004.
- [9] S. Murakami, K. Bogaki, T. Tanaka, H. Hayama, Y. Yoshino, S. Akabayashi, T. Inoue, A. Iio, S. Hokoi, A. Ozaki, Y. Ishiyama, Y.,2006. Detail survey of long-term energy consumption for 80 houses in principle cities of Japan – Description of the houses and end use structure of annual energy consumption. Architectural Institute of Japan 603, 93– 100.
- [10] R. Hendron and J. Burch, Development of Standardized Domestic Hot Water Event Schedules for Residential Buildings, Presented at Energy Sustainability 2007, Long Beach, California Jun 27–30, 2007 <u>http://dx.doi.org/10.1115/es2007-36104</u>
- [11] A. Lowenstein, and C. Hiller, 1996, "Disaggregating Residential Hot Water Use," ASHRAE Transaction Symposia, January 1996, Atlanta, GA: ASHRAE.
- [12] C. Aguilar, D.J. White, and David L. Ryan, Domestic Water Heating and Water Heater Energy Consumption in Canada, April 2005, CBEEDAC 2005–RP-02.
- [13] B. Bøhm, PO. Danig. Monitoring the energy consumption in a district heated apartment building in Copenhagen, with specific interest in the thermodynamic performance. Energy Build 2004;36:229–36. http://dx.doi.org/10.1016/j.enbuild.2003.11.006
- [14] F. Schrøder, Cirkulationstab i varmt brugsvandsanlæg er langt større end antaget (Circulation heat losses much bigger than previously estimated). Danish HVAC J 2004;4:36–40.
- [15] European Parliament and Council of the European Union 2010. Directive 2010/31/EU of the European Parliament and the Council of 19 May 2010 on the energy performance of buildings (recast). Official Journal of the European Union L 153/13-35 of 18.6.2010.
- [16] European Parliament and Council of the European Union 2002. Directive 2002/91/EC of the European Parliament and the Council of 16 December 2002 on the energy performance of buildings. Official Journal of the European Communities L 1/64-71 of 4.1.2003.
- [17] EN 15316-1 Heating systems in buildings Method for calculation of system energy requirements and system efficiencies – Part 1: General.
- [18] J. Zirngibl, Information paper on EN 15316-1 Heating systems in buildings - Method for calculation of system energy requirements and system efficiencies – Part 1: General, IEE-CENSE, European Communities, 2009.
- [19] Compilation of Information Papers introducing the CEN standards concerning Heating Systems and Domestic Hot Water - Booklet 3: Heating and DHW Systems, IEE-CENSE, European Communities, 2010.
- [20] H. van Wolferen, Information paper on EN 15316-3-1 Domestic Hot Water systems - Characterisation of Needs (tapping requirements), IEE-CENSE, European Communities, 2008.
- [21] EN 15316-3-1 Heating systems in buildings Method for calculation of system energy requirements and system efficiencies - Part 3-1: Domestic hot water systems, characterisation of needs (tapping requirements).

- [22] EN 15316-3-2 Heating systems in buildings Method for calculation of system energy requirements and system efficiencies - Part 3-2: Domestic hot water systems, distribution.
- [23] H. van Wolferen, Information paper on EN 15316-3-2 Domestic Hot Water systems - Distribution, IEE-CENSE, European Communities, 2008.
- [24] Statistics Database, ENG08. ENERGY BALANCE, thsd toe (NACE Rev.2). Central Statistical Bureau of Latvia, data.csb.gov.lv.
- [25] R. Burzynski, M. Crane, R. Yao, A review of domestic hot water demand calculation methodologies and their suitability for estimation of the

demand for Zero Carbon houses, TSBE EngD Conference, TSBE Centre, University of Reading, Whiteknights Campus, RG6 6AF, 6th July 2010, http://www.reading.ac.uk/tsbe/.

[26] F.S. Goldner, "Energy Use and Domestic Hot Water Consumption", New York State Energy Research and Development Authority, Report 94-19, 1994.